



# Pipe Network Modelling for Urban Inundation

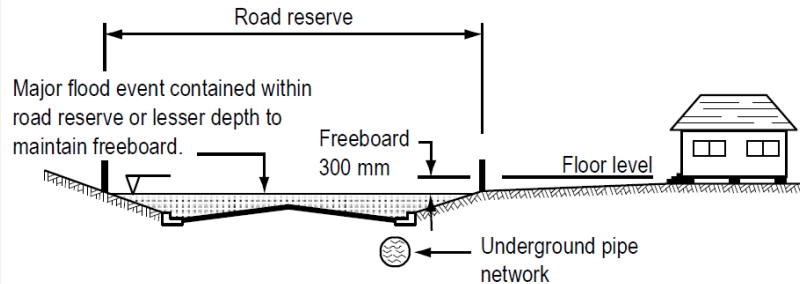
Bill Syme and Chris Huxley



# Today's Presentation Overview

## Focus on pipe network modelling for modelling urban inundation

- 1<sup>st</sup> half on key theory – Bill Syme
- 2<sup>nd</sup> half on practical and quality control considerations – Chris Huxley



**Building above top of kerb and channel**

*Qld Urban Drainage Manual (QUDM), 2016*



Pipe Network Modelling for  
Urban Inundation

# Theory

# Theory Overview

## Topics

- Pipe flow regimes
  - Friction
  - Junctions / Manholes
- Energy losses
- Overland flow capture
- Surcharging
- Blockages
- Operational structures





# Theory

## Some Terminology

### Velocities ( $V$ ), for example

- $V_i$  = Velocity in inflow pipe
- $V_o$  = Velocity in outflow pipe

### HGL ( $H$ )

- HGL (Hydraulic Grade Line)
  - Water level (for full pipe, the level in a vertical tube inserted in top of pipe)
- *Total Energy* =  $H + V^2/2g$

### Energy Loss Coefficient ( $K$ )

- The fraction of lost kinetic energy ( $V^2/2g$ )

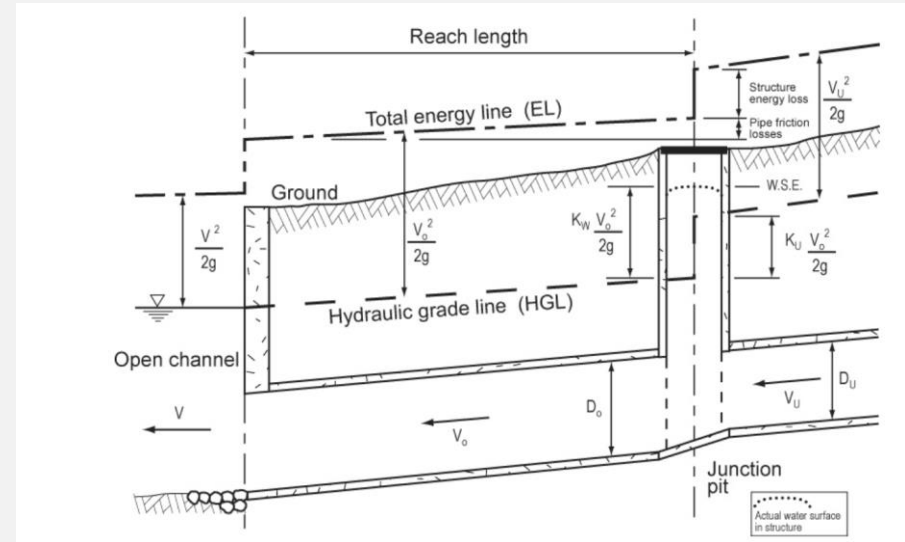


Figure 7.16.1 Qld Urban Drainage Manual (QUDM), 2016

# Pipe Flow Regimes

## Outlet Controlled

### Outlet Controlled Flow Occurs Where

- Downstream water level influences the flow rate
  - Flow is subcritical or pressurised
  - Inlet and outlet energy and friction losses apply
- Free outflow (critical flow) at outlet
  - Inlet energy and friction losses apply

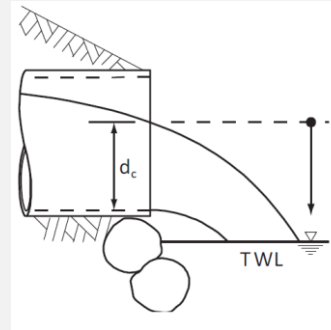
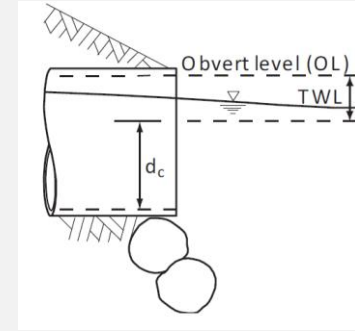
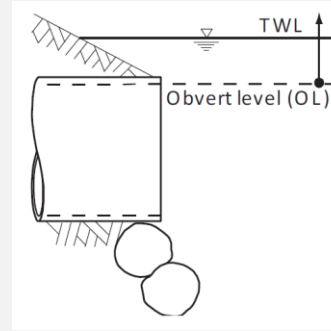


Figure 7.16.2 Qld Urban Drainage Manual (QUDM), 2016

# Pipe Flow Regimes

## Inlet Controlled

### Inlet Controlled Flow Occurs Where

- Inlet conditions control the flow rate
  - Super-critical flow
  - Sufficiently steep to transition into critical flow
  - Orifice flow transitions into critical flow

### Note

- Downstream conditions have no affect on flow rate
- Entrance and exit energy losses not applicable

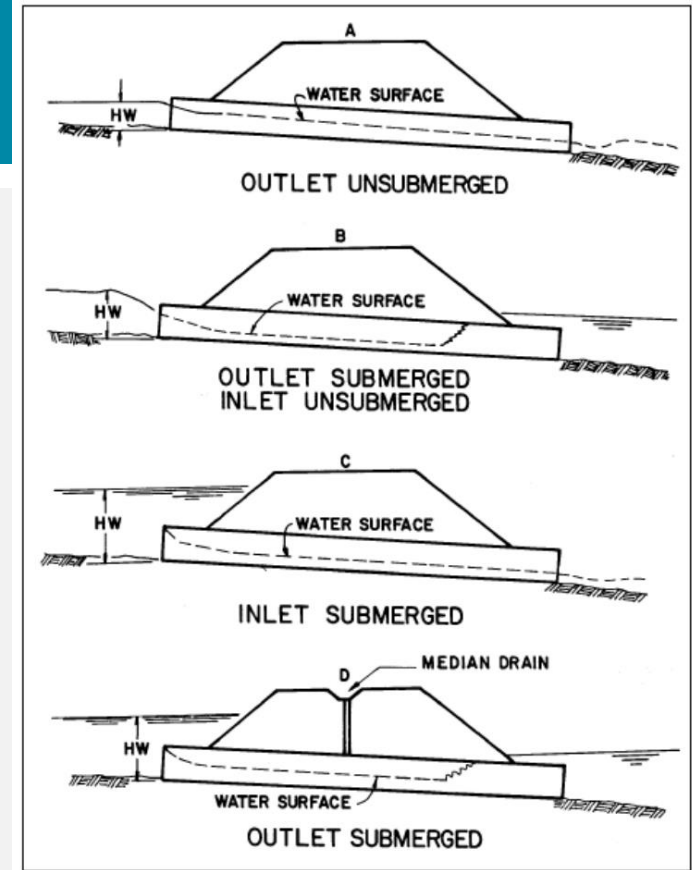


Figure III-1 HEC Hydraulic Design Charts

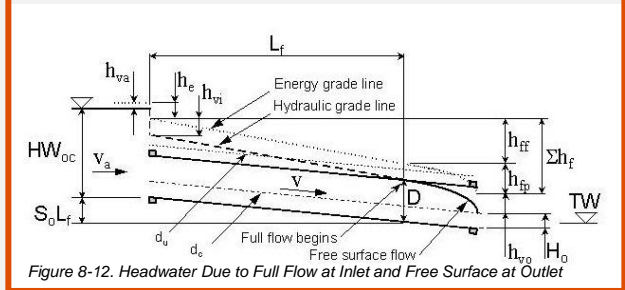
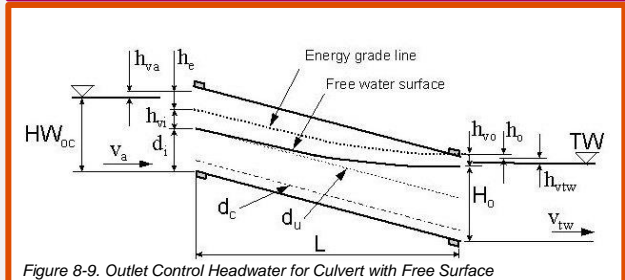
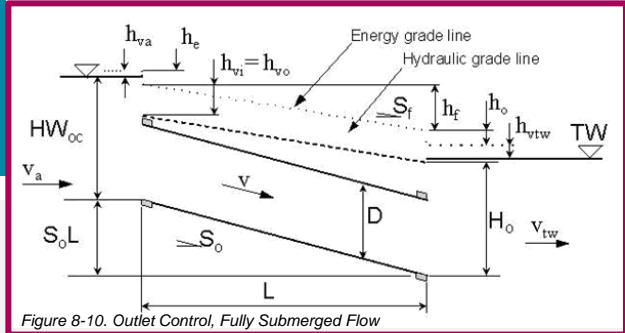
# Friction Energy Losses

## Manning's Equation

$$\Delta H_f = S_f L$$

### Manning's equation

- $\Delta H_f = \left( \frac{nV}{R^{2/3}} \right)^2 L$  or  $Q = \frac{AR^{2/3}}{n} \sqrt{\frac{\Delta H_f}{L}}$
- $n$  is Manning's coefficient;  $R = A/P$
- Straightforward calculation when pipe flowing full
  - $R$  is fixed at  $\frac{A}{P} = \frac{\pi r^2}{2\pi r} = \frac{r}{2}$
- Pipe partially full – an open channel flow problem (not so straightforward – indeterminate equation)



[http://onlinemanuals.txdot.gov/txdotmanuals/hyd/manual\\_notice.htm](http://onlinemanuals.txdot.gov/txdotmanuals/hyd/manual_notice.htm)



# Friction Energy Losses

## Manning's n Values

### Plenty of guidance in literature



Nature of Surface	Manning's n Range
Concrete Pipe	0.011 – 0.013
Corrugated Metal Pipe	0.019 – 0.030
Vitrified Clay Pipe	0.012 – 0.014
Steel Pipe	0.009 – 0.011
Monolithic Concrete	0.012 – 0.017
Cement Rubble	0.017 – 0.025
Brick	0.014 – 0.017
Laminated Treated Wood	0.015 – 0.017
Open Channels	
Lined with Concrete	0.013 – 0.022
Earth, clean, after weathering	0.018 – 0.020

In: Viessman and Hammer. *Water Supply and Pollution Control, Sixth Edition*. 1998. (Table 6.1) Adapted from: *Design Charts for Open-Channel Flow*. U.S. Department of Transportation, Federal Highway Administration, Hydraulic Design Series No. 3, U.S. Government Printing Office, Washington, D.C. 1961.

R Pitt, S Clark: *Flow in Pipes, Manning's Equation presentation*

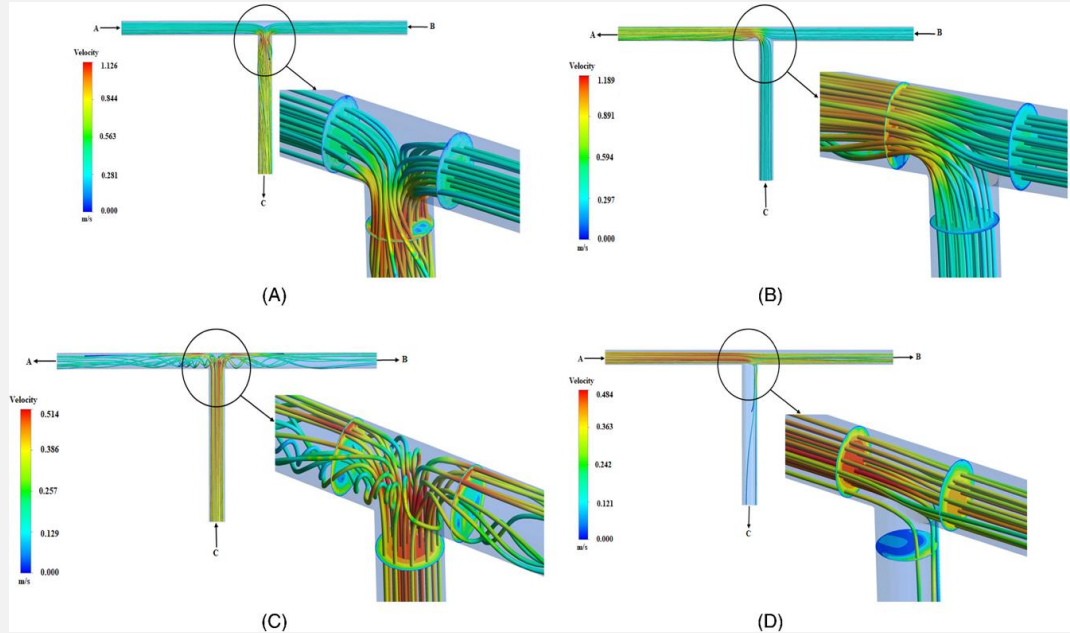
# Kinetic Energy Losses

## Manholes, Junctions, Bends, Obstructions

$$\Delta H = K \frac{v^2}{2g}$$

- Fraction ( $K$ ) of kinetic energy loss

**Manholes most common**  
(and most hydraulically complex!)



*B.D. Gajbhiye et al, Teaching turbulent flow through pipe fittings using computational fluid dynamics approach, Jan 2020*  
<https://onlinelibrary.wiley.com/doi/10.1002/eng2.12093>

# Kinetic Energy Losses Manholes

## Primary functions

- Access for construction or maintenance
- Accommodate pipe transitions/changes
- Receive flow from above ground inlets

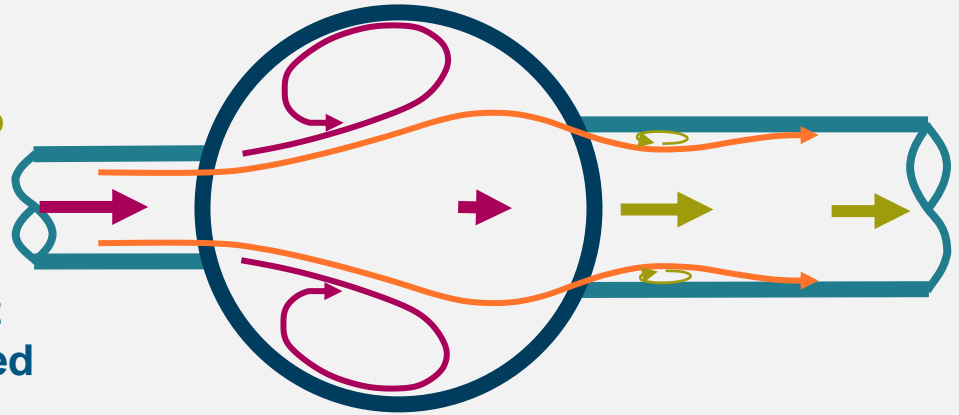


# Kinetic Energy Losses Manholes

## Manhole kinetic energy losses

- Expansion of inlet flows
- Expansion of flow downstream of outlet due to
  - Formation of a vena-contracta in an outlet pipe
  - Discharging into a receiving water body

**Note:** Above energy losses are relevant if a pipe is flowing in an outlet controlled flow regime



# Kinetic Energy Losses Manholes

## Additional kinetic energy losses

- Change in horizontal alignment
- Change in vertical alignment
- Other effects such as kerb inlet flows if a significant % of total flow

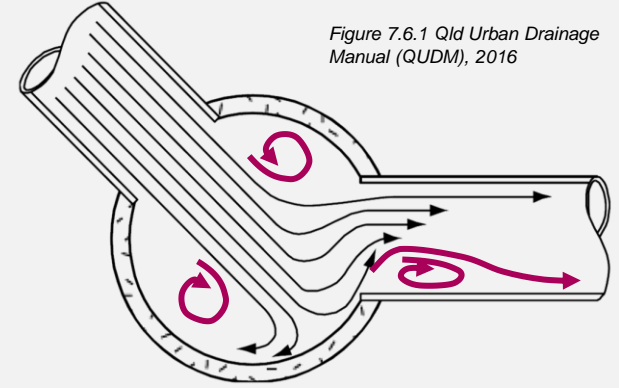
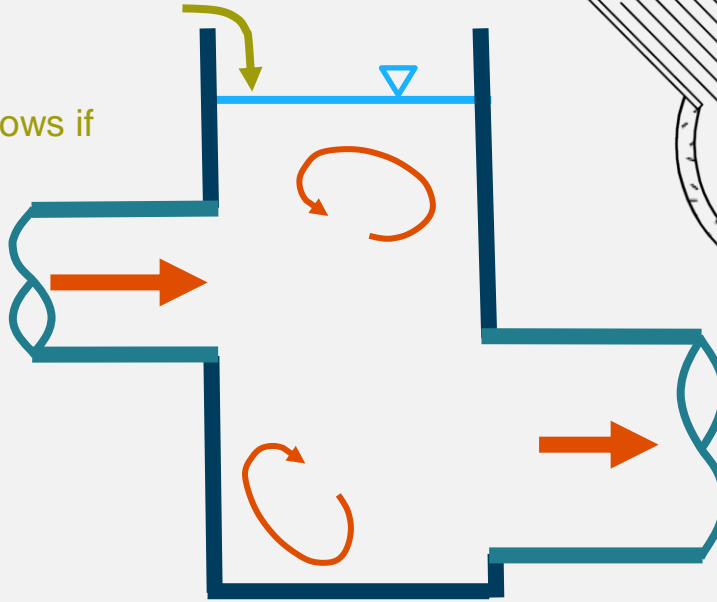
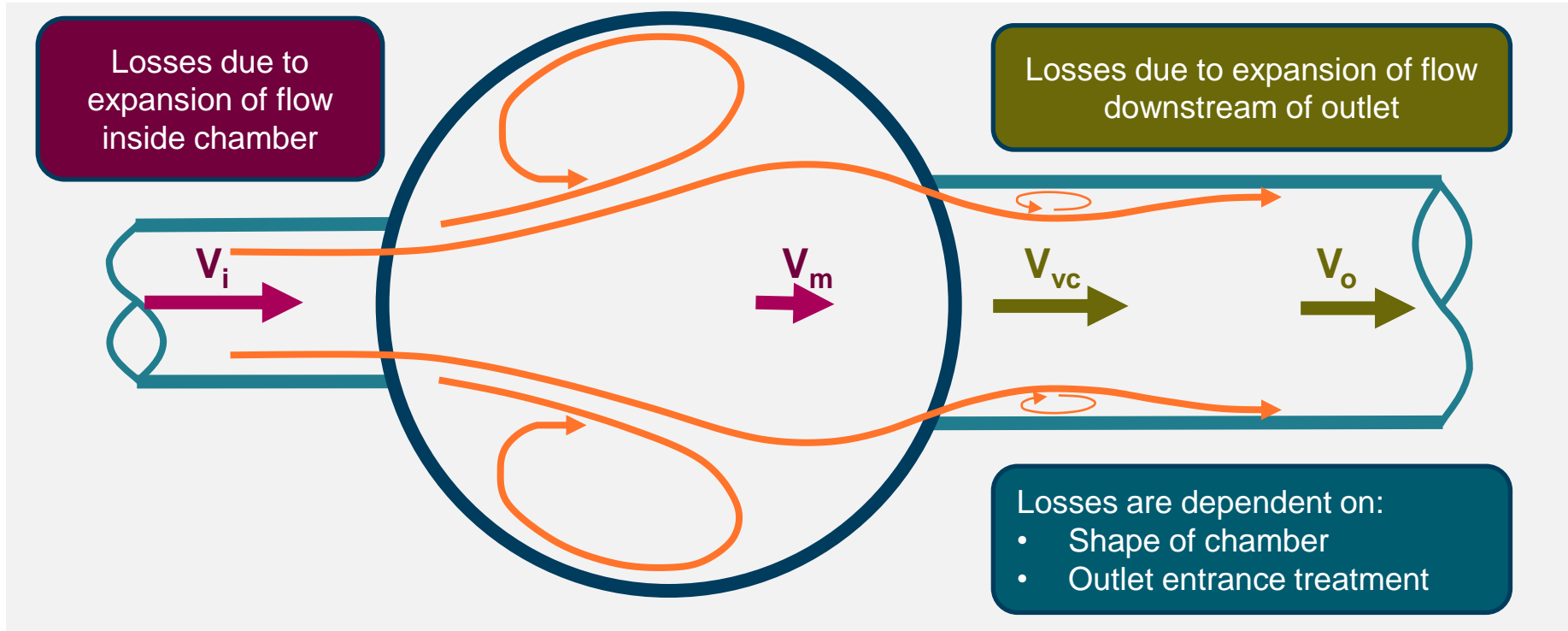


Figure 7.6.1 Qld Urban Drainage  
Manual (QUDM), 2016

# Kinetic Energy Losses

## Manhole Inlet and Outlet Losses





# Energy Losses

## Manholes – Modelling Approaches

### Fix K

- Derived from
  - Desktop calculations
  - Flume or field measurements
- If K varies with flow, not ideal for dynamic simulations
- Plenty of values in the literature
- Be careful as to which velocity K applies to (Total K usually based on outlet velocity,  $V_o$ )**

### Vary K according to conditions

- Uses equations for different loss components
- Suits dynamic solutions – recalculate K each timestep

Table 7.16.7 – Energy loss coefficients for flow expansions and contractions within pipes<sup>[1]</sup>

$A_U/A_O$ or $A_O/A_U$	d/D	Sharp expansion <sup>[2]</sup>	Contraction <sup>[3]</sup>				
			Sharp edge	r/d = 0.02	r/d = 0.04	r/d = 0.06	r/d = 0.1
1	1.000	0.000	0.000	0.000	0.000	0.000	0.000
0.8	0.894	0.081	0.079	0.058	0.043	0.036	0.027
0.6	0.775	0.200	0.248	0.165	0.121	0.091	0.060
0.4	0.632	0.377	0.371	0.255	0.187	0.137	0.077
0.2	0.447	0.659	0.442	0.324	0.234	0.169	0.086
0.1	0.316	0.833	0.471	0.353	0.245	0.180	0.087
0	0.000	1.000	0.500	0.376	0.250	0.185	0.087

Notes:

[1] Sourced from Miller (1990).

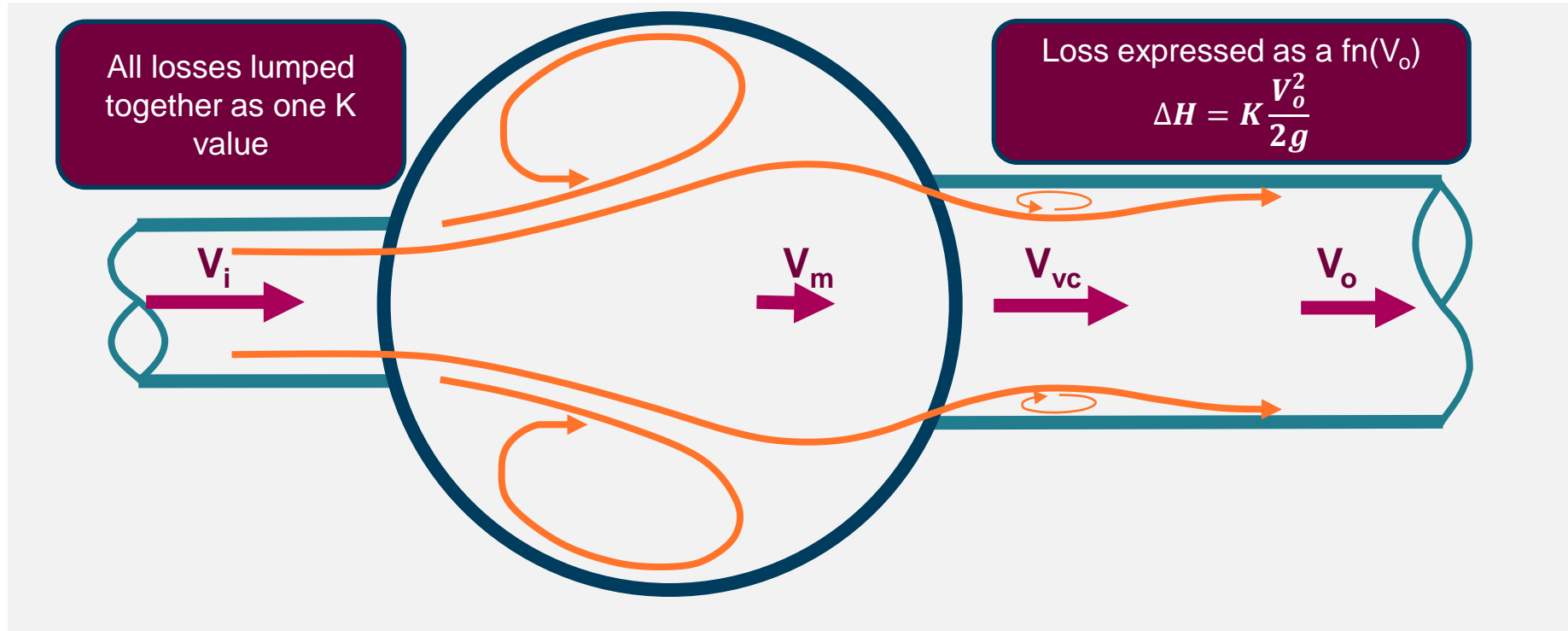
[2] Energy loss coefficient ( $K_{exit}$ ) relative to upstream velocity head ( $V_U^2/2g$ ).

[3] Energy loss coefficient ( $K_{entry}$ ) relative to downstream velocity head ( $V_O^2/2g$ ).

Table 7.16.7 Qld Urban Drainage Manual (QUDM), 2016

# Energy Losses

## Manholes – Fixed K Approach



# Energy Losses

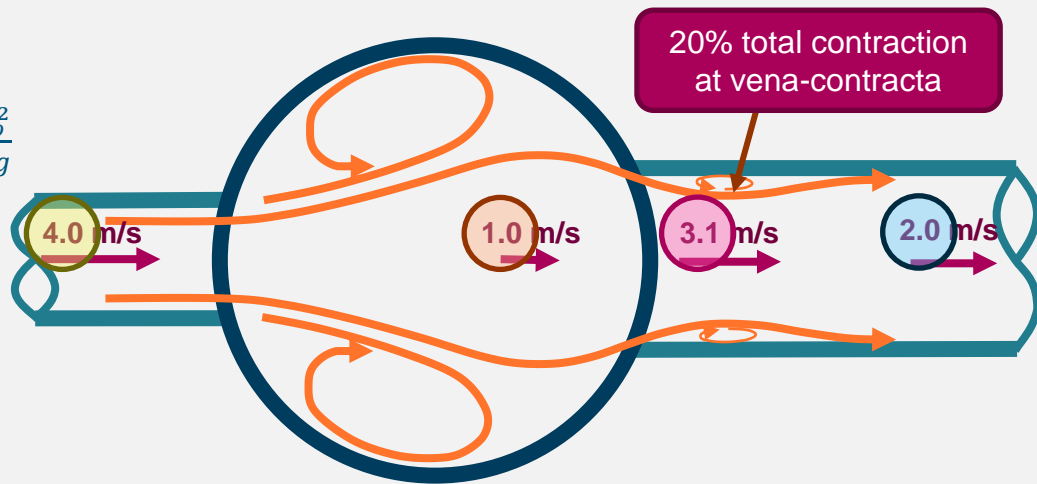
## Manholes – Fixed K Desktop Example

Assuming only inlet and outlet losses (pipes are aligned)

- Expansion loss (derived from first principles) =  $\frac{(V_{us}-V_{ds})^2}{2g} = \left(1 - \frac{V_{ds}}{V_{us}}\right)^2 \frac{V_{us}^2}{2g}$
- Inlet loss =  $\Delta H_i = \left(1 - \frac{4.0}{1.0}\right)^2 \frac{V_i^2}{2g} = 0.56 \frac{V_i^2}{2g}$
- Outlet loss =  $\Delta H_o = \left(1 - \frac{3.1}{2.0}\right)^2 \frac{V_o^2}{2g} = 0.13 \frac{V_o^2}{2g}$

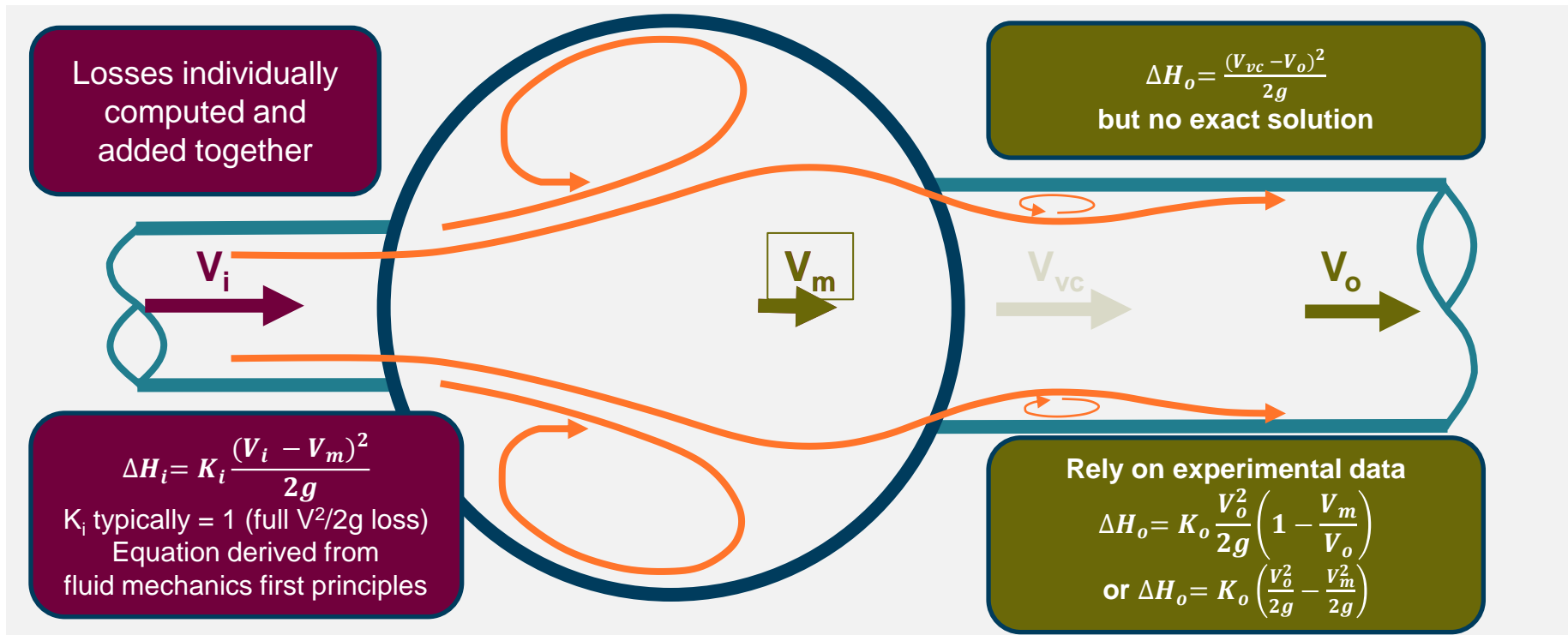
Let's base energy loss on  $V_o$  (2 m/s)

- $\Delta H = K \frac{V_o^2}{2g} = \Delta H_i + \Delta H_o$
- $K = \frac{2g}{V_o^2} (\Delta H_i + \Delta H_o) = 0.56 \frac{V_i^2}{V_o^2} + 0.13$
- $K = 2.4$**  (note,  $K \neq 0.56 + 0.13$ )



# Energy Losses

## Manholes – Variable Energy Loss Approach



# Additional Energy Losses

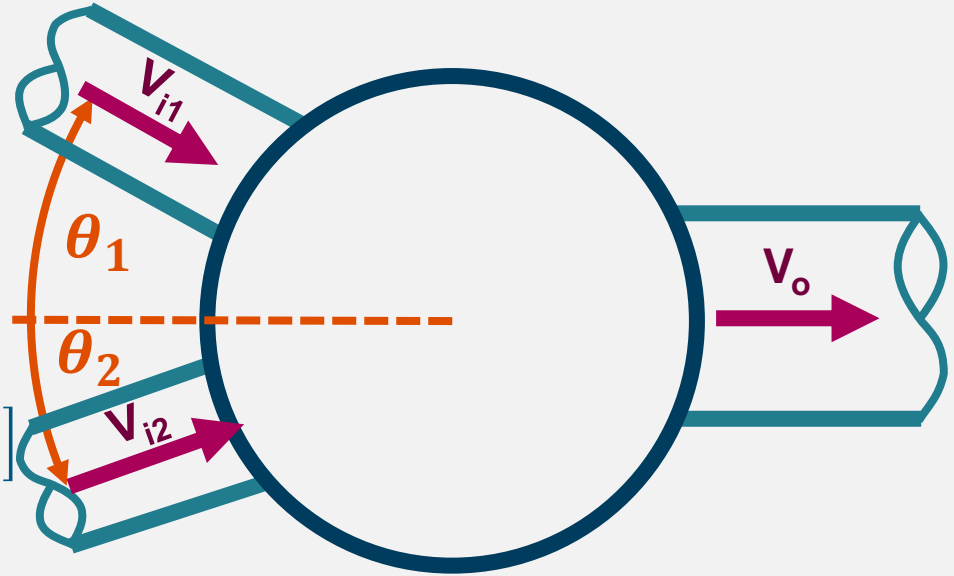
## Manholes – Variable Energy Loss Approach

### Unaligned pipe losses

- Angle of approach differs to outflow pipe(s)
- Handles multiple inflow pipes
- $K_{\theta} = \sum_i \left[ f_i \min \left( \frac{\theta_i^2}{90^2}, 4 \right) \right]$
- $f_i = \frac{Q_i}{\sum Q_o}$  (fraction of total flow)

### Change in pipe invert elevations

- $K_z = \sum_i \left[ \min \left( \max \left( \frac{f_i(h_o - h_i)(h_o + y_o - h_i - y_i)}{y_o y_i}, 0 \right), 2 \right) \right]$



# Minimising Energy Losses Manholes

## Maintain velocities through manhole

- Keeping chamber size to minimum
- Minimise turbulence/eddies
- Benching

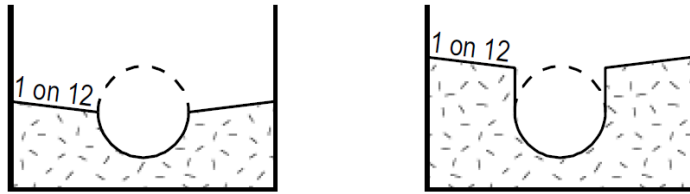


Figure 7.16.4 Qld Urban Drainage Manual (QUDM), 2016

## Minimise vena-contracta effect in outlet pipe

- e.g. using Bellmouth entrance

Direct flow to  
centre of outlet

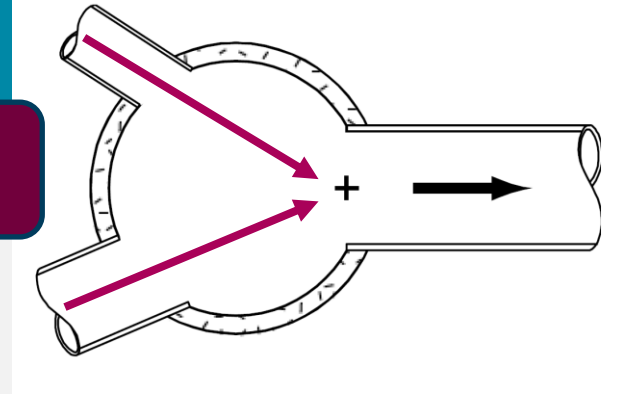


Figure 7.6.2 Qld Urban Drainage Manual (QUDM), 2016

Maximise  
vena-contracta width  
(to reduce  
vena-contracta  
velocity)

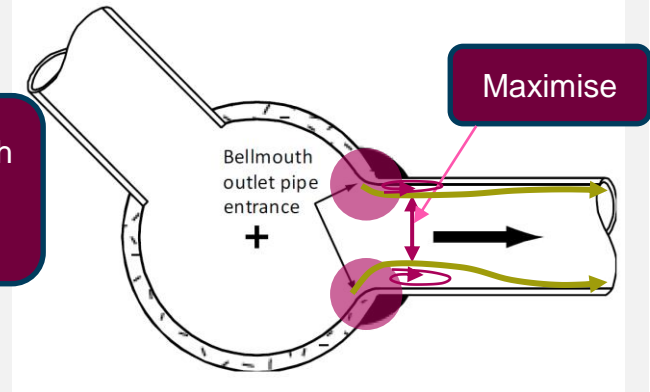


Figure 7.6.3 Qld Urban Drainage Manual (QUDM), 2016



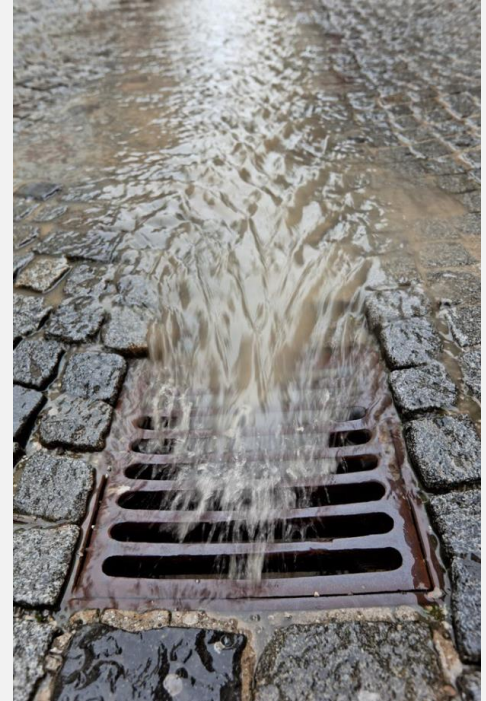
# Above Ground Flow Capture Inlets/Pits/Drains/Gully Traps

**Captures road or overland flow into pipe network**

- Many, many approaches!
- May also backflow or surcharge (intentionally or unintentionally!)

**Different terminologies, same function**

- Pits
- Inlets / Kerb inlets
- Drains
- Gully traps



# Above Ground Flow Capture On-Grade Kerb Inlets

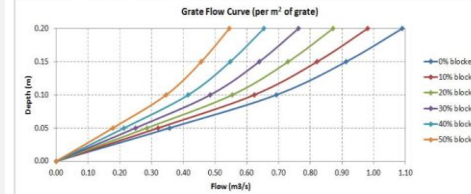
## Drains water from road kerbing

- Flow higher flows, bypass flow occurs (Steeper the road, greater the bypass flow)
- Use approach flow vs capture flow (Q-Q), or depth vs capture flow (y-Q) curves
  - Derived from flume/field measurements or theory
  - Can convert Q-Q to a y-Q curve using Manning's equation

**Critical to have accurate representation of above ground depth or approach flow**

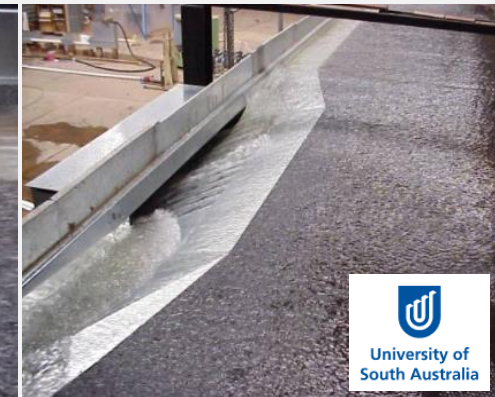
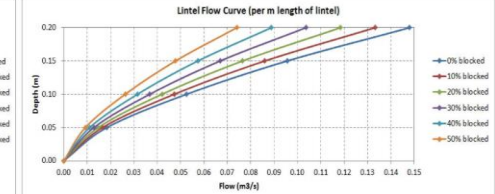
Water Depth (m)	0% blocked	10% blocked	20% blocked	30% blocked	40% blocked	50% blocked
0.00	0.000	0.000	0.000	0.000	0.000	0.000
0.05	0.304	0.321	0.340	0.360	0.374	0.379
0.10	0.693	0.624	0.564	0.486	0.416	0.347
0.15	0.913	0.822	0.730	0.639	0.548	0.456
0.20	1.089	0.980	0.871	0.763	0.654	0.545

NOTE: Multiply table value by grate area to calculate site specific value



Water Depth (m)	0% blocked	10% blocked	20% blocked	30% blocked	40% blocked	50% blocked
0.00	0.000	0.000	0.000	0.000	0.000	0.000
0.05	0.010	0.010	0.010	0.010	0.010	0.010
0.10	0.013	0.013	0.013	0.013	0.013	0.013
0.15	0.016	0.016	0.016	0.016	0.016	0.016
0.20	0.018	0.018	0.018	0.018	0.018	0.018

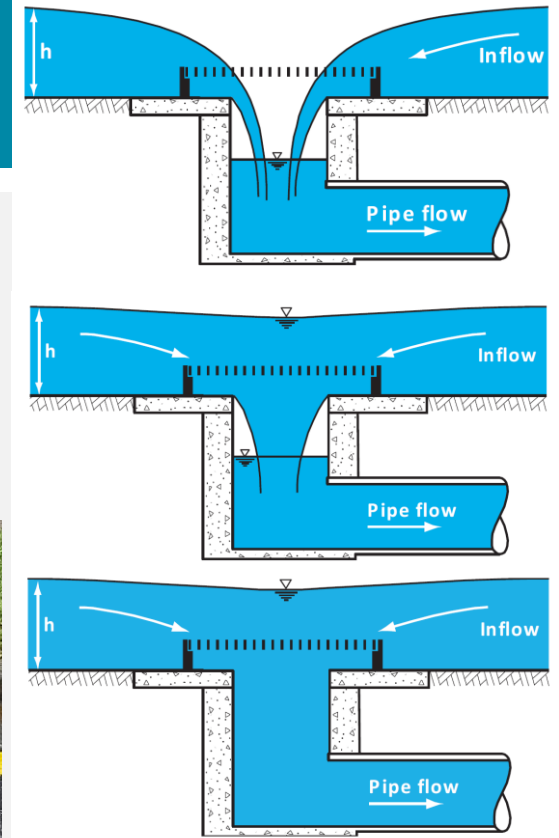
NOTE: Multiply table value by lintel length to calculate site specific value



# Above Ground Flow Capture Sag Inlets

## Drains ponded water

- Best modelled using depth-discharge relationship
  - Derived from flume/field measurements or theory
- Assume no bypass flow
- High probability of debris impeding flow



Figures 7.5.4, 7.5.5, 7.5.6  
Qld Urban Drainage Manual (QUDM), 2016



# Flow Surcharging Inlet Backflow

**Backflow occurs where pipe pressure (head) exceeds ground level**

- Often cause of unintentional flooding

## Causes

- Pipe design capacity exceeded
  - Which maybe the intended design, for example
    - Pipes designed for 1 in 10 AEP
    - Roadways and overland flow paths > 1 in 10 AEP
- Blockage in the pipe network
- Backflow from receiving waters
  - River in flood or elevated tidal levels

## May need different y-Q curve to capture flow

- If ground flooded, backflow flow rate may be controlled by ground flood depth



# Flow Surcharging Manhole Lid Popping

## Manhole lid popping

- Usually unintended – pressure exceeds downward forces
- Suddenly causes backflow
- Modelling requires conditions around when lid will pop



# Blockages

## Major problem, managed via

- Trash racks and gross pollutant traps
- Debris deflectors
- Maintenance programs

Table 7.5.1 – Provision for blockage at kerb inlets

Inlet type	Blockage factor	
	Design value <sup>[1]</sup>	Severe conditions <sup>[2]</sup>
<b>Sag kerb inlets:</b>		
Kerb inlet	20%	100 %
Grated	50 %	100%
Combination	[3]	100%
<b>Continuous (on-grade) kerb inlets:</b>		
Kerb inlet	20%	100%
Longitudinal bar grated	40%	100%
Transverse bar grate or longitudinal bar grate incorporating transverse bars	50%	100%
Combination	[4]	100%
<b>Field (drop) inlets:</b>		
Flush mounted	80%	100%
Elevated (pill box) horizontal grate	50%	100%
Dome screen	50%	100%
Open pipe inlets (blockage factors as per culverts)	Refer to Table 10.4.1	

Table 7.5.1 Qld Urban Drainage Manual (QUDM), 2016





# Operational Structures

## Example

- Backflow prevention devices
- Pumps
- Gates

## Upcoming Webinar

### Operational Structure Modelling using TUFLOW

Presenters: Phillip Ryan  
and Dr Shuang Gao

April 13, 2022



Pipe Network Modelling for  
Urban Inundation

# Hands-on Modelling Quality Control Discussion / Demonstration